Advanced Reactor Technology-Supercritical Carbon Dioxide Brayton Cycle R&D

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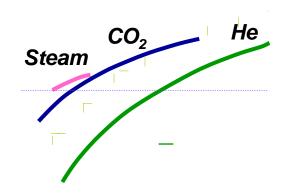
Sandia National Laboratories

NRT Summit March 22, 2012



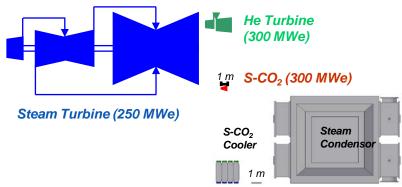
S-CO2 Turbomachinery Demonstration Program Objectives

- Highest thermal/electrical conversion efficiency
- Demonstrate Super-Critical Carbon Dioxide (S-CO2) Brayton cycle capability
- Demonstrate up to 50% conversion efficiency
- 1/10 of the System volume
- 1/100th of the cost



Rejects Heat
Above Critical Point
High Efficiency Non-Ideal Gas
Sufficiently High for Dry Cooling

Critical Point 88 F / 31 C 1070 psia / 7.3 MPa

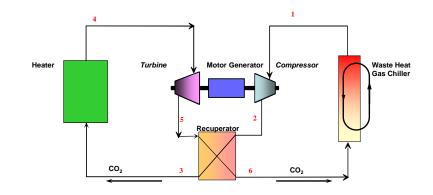




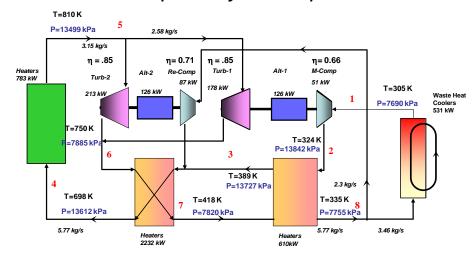
Brayton Cycle History

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- 2005 Sandia demonstrated a closed Brayton cycle using gases for space propulsion,
- 2007 initial investigation into the stability of S-CO₂ as a working fluid very near the fluid's critical point – a thermodynamic state in which fluid properties vary dramatically.
- 2009 DOE funded development of a series of more extensive test article
 - S-CO2 Compressor Loop
 - S-CO2 Simple Brayton Loop
 - S-CO2 Split-Flow, Fully recuperated, Recompression Brayton Loop
- 2009 Developed Compressor Maps for various gases and mixtures
- 2010 Demonstrated operation of the Simple Brayton Cycle
- 2011 Demonstrated operation of the Split-Flow Brayton Cycle.
- March 2012 Shipment of Split Flow Loop to Sandia



Simple Brayton Loop



Split-flow, Fully Recuperated, Recompression Brayton Loop



Sandia S-CO2 Brayton Loops

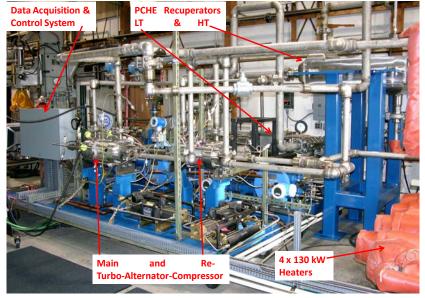
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- Two Turbine-Alternator-Compressors (TAC's) designed to produce 125 kW of electricity each,
- A bank of heaters with 780 kW capacity,
- Two recuperators to transfer heat from the high temperature flow exiting the turbine to the low temperature flow exiting the compressors, and
- A heat rejection heat exchanger.





Low Pressure Simple Brayton Loop



S-CO2 Split Flow Brayton Loop



Specialty training at Barber Nichols before loop delivery

TAC teardown

- Complete disassembly of TAC A and B
- Used for trouble shooting various turbo machinery problems
 - i.e. failed bearings, break away torque out of spec., rubbed turbo machinery...
- Developed SNL-OP-TT001 which is a procedure to disassemble the TAC unit

■ TAC clearance adjustment

- Several crucial adjustments are present in each TAC unit
 - i.e. turbine, compressor, and recompressor clearance from respective shrouds.
- Developed SNL-OP-CT001 which is a procedure to verify the clearances in both TAC units

TAC assembly

- Complete assembly of TAC A and B
- Used for replacing various turbo machinery components
 - i.e. failed bearings, rubbed turbo machinery, shrouds, and sensors...
- Developed SNL-OP-AT001 which is a procedure to assemble the TAC unit









Expedited Schedule

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March 19th -23st

BNI

Acceptance testing of completed test article at March 22nd- 30th

Complete disassembly, packaged for shipment and shipment

April 2nd– June 29th

Assembly and commissioning of newly installed SCO2 Brayton loop

February $20th - 24^{th}$ March

completed

12th - 16th Final loop upgrades

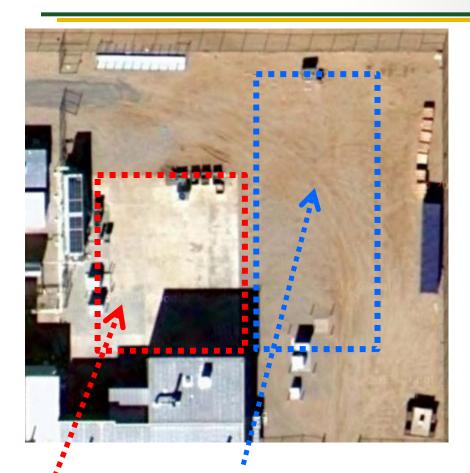
TAC disassembly and reconfiguration

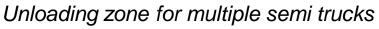




Delivery and Construction

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Staging area for off loaded equipment



S-CO2 Brayton Cycle

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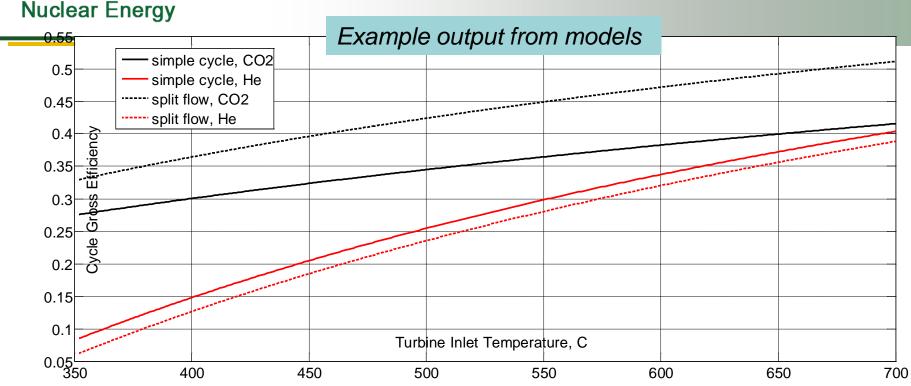
- Major system upgrades are nearly completed to attain the original testing capabilities of:
 - 75,000 RPM on both Turbo-Alternator-Compressor (TAC) units.
 - 780 kWth input power.
 - Peak operating temperature of 1000°F.
 - Peak operating pressure of 18.7 MPa.
 - 5.7 kg/sec mass flow rate.
 - Net power generation on the order of 250 kWe.
- Recent focus has been to:
 - Complete upgrades.
 - Perform acceptance testing of the upgraded test article (TA) at the contractor facility.
 - Prepare test facility site at Sandia, Albuquerque (see photos at right).
 - Transport the TA from the contractor facility to Sandia Albuquerque.
 - Perform commissioning tests on the TA to verify functionality.
 - Open the Nuclear Technology Users Facility (NTUF) for commercial component demonstration testing.



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Recent Modeling Accomplishments



- Modeling tools developed that can predict Brayton cycle gross efficiency for any combination of the following variables.
- Simple or split flow configuration
- Heat rejection temperature (low temperature)
- Turbine inlet temperature (high temperature)
- Compressor inlet pressure (low pressure)
- Compressor discharge pressure (high pressure)

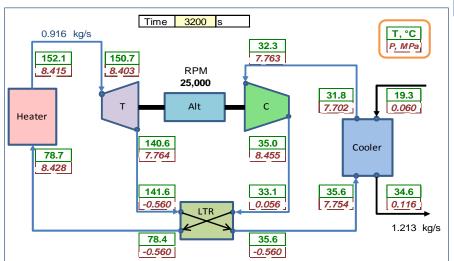
- Recuperator efficiencies
- Turbine and compressor efficiencies
- Component pressure drop
- Working fluid

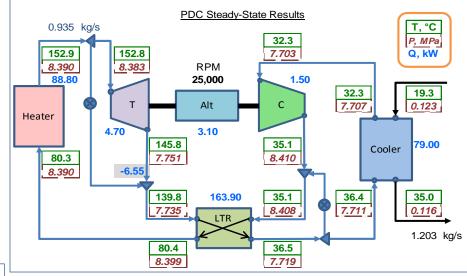


Steady-State Results

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- The results of the steady-state calculations from the Plant Dynamics Code (PDC) model are surprisingly close to the experimental data
 - Pressures, temperatures, flow rates
 - Despite all the uncertainties of the experimental data
 - Special adjustments for heat loss were needed





Experimental Data

Code Prediction



Analysis of SCO₂-Lubricated Bearings

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Background

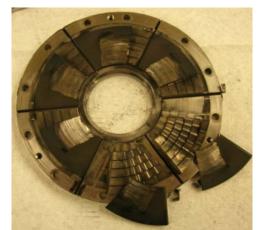
- SNL has developed flow loops for demonstrating the feasibility of the S-CO₂ Brayton cycle.
- The loops are driven by turbomachinery running on gas foil journal and thrust bearings.
 - Gas bearings provide oil-free radial and axial support at high temperatures and speeds, and are an 'enabling technology' for microturbine systems such as the SNL facilities
 - But they are an emerging technology with few manufacturers and little performance data available

• Problem and Proposed Solution:

- Models for power loss and thrust load capacity for compliant foil bearings do not exist, yet
 these are of great importance in understanding operating limits of the Brayton cycle hardware.
- Thrust bearings analysis codes validated by experimental data are needed to understand the impact of operational parameters on bearings performance

This work will allow the DOE S-CO₂ Brayton loop to generate more electricity, at higher efficiency.

- Currently the loop is limited by thrust bearing performance: 60,000 rpm has been reached, short of the 75,000 rpm design point
- Mechanisms to decrease frictional heating while maintaining load capacity will soon be needed.



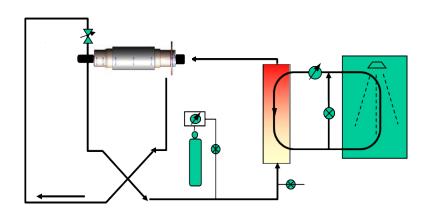


Experimental Thrust Bearings Test Rig

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A thrust bearings test rig has been built in Bldg 6630 at SNL

- Advanced bearings designs are currently being evaluated for potential to reduce friction
- Load capacity, friction are being measured for different operating conditions
- Data will benchmark the code, allowing the model to be used for design of upgraded bearings in the near future.
- Also, successful performance of the new bearings on the test rig will prove they are able to support thrust loads on the DOE SCO₂ Brayton cycle test loop





Pictured: Failure of an advanced thrust bearing design

• FY12 Goals:

- Characterize thrust loads during typical SCO₂ Brayton loop startup/shutdown transients to confirm that the new bearings can support maximum expected loads.
- Conduct further experimental tests for a range of speeds 25000-75000 rpm, bearings pressures from 200-800psi, loads of 100-400lbs



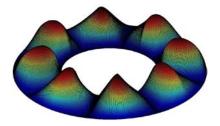
Thrust Bearings Modeling

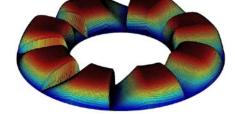
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- A new code has been developed for analysis of compliant thrust bearings
 - Isothermal elastohydrodynamic model has created by evaluating the turbulent Reynolds Eqn.
 - Code solves for fluid velocity field, load capacity and frictional power loss, is linked to NIST RefProp for dynamic updating of CO₂ fluid properties

$$\frac{1}{\overline{r}}\frac{\partial}{\partial \overline{r}}\left(\overline{r}G_{r}\overline{\rho}\overline{h}^{3}\frac{1}{\overline{\mu}}\frac{\partial\overline{p}}{\partial \overline{r}}\right) + \frac{1}{\overline{r}^{2}}\frac{\partial}{\partial\theta}\left(G_{\theta}\overline{\rho}\overline{h}^{3}\frac{1}{\overline{\mu}}\frac{\partial\overline{p}}{\partial\theta}\right) = \Lambda\frac{\partial\left(\overline{\rho}\overline{h}\right)}{\partial\theta}$$

- The code has been successful in explaining unexpected phenomena observed during experiments
 - Modeling has shown that the lubrication layer is in the highly turbulent regime, accounting for the very sensitive relationship between friction and lubricant density observed
 - The high-rpm saturation of load capacity has been explained by the profile of the building lubrication pressure at the thrust pads.





Pictured: Pressure profiles of a thrust bearing evaluated using the new code

Low rpm

High rpm

FY12 Goals:

 Add temperature dependence to the fluid/structure models, work on comparison of the simulated results to experimental data.

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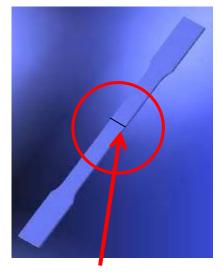
Heat Exchanger program

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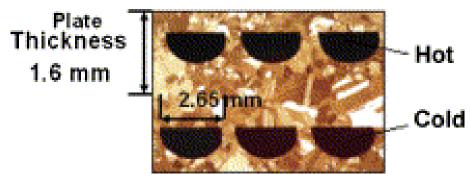
Prepare a Federal Business Opportunity (In process)

Select contractor

- Fabricate ASTM stress coupons to validate diffusion bonding as a structural support mechanism. Validation will take place on an Instron machine output results σ vs. ε
- Fabricate NQA1 printed circuit heat exchangers. Idea is to fabricate one large diffusion bonded heat exchanger (4'x4'), separate into 16 separate heat exchangers and make necessary manifold connections so they can perform as 16 heat exchanges separately.
- At site host hydro test to failure each heat exchanger to investigate failure mechanisms of the heat exchangers.
 Also investigate the sodium to SCO2 interface within the heat exchanger.



ASTM sample to test strength of Diffusion Bonding





Metal Corrosion in Supercritical CO₂ and Liquid Sodium

- A review report titled: Metal Corrosion in a Supercritical Carbon Dioxide Liquid Sodium Power Cycle has been completed and submitted.
- The report consisted of a gap analysis that identified the following areas for additional work:
 - Corrosion testing in supercritical CO₂ needs to be performed with metal coupons under stress. Experience gained with the operation of the Magnox CO₂ cooled reactors indicates the most severe corrosion was observed for components under stress.
 - The effects of water, oxygen and other impurities need to be examined in more detail. The literature indicates water at ppm concentrations creates a very corrosive environment for many metals in the presence of CO₂.
 - Tests need to be performed for diffusion bonded materials in liquid sodium. No information is available in the literature on this topic.
 - Additional testing at high temperatures, 300 600°C, needs to be performed to understand the mechanism of carburization in liquid sodium as this will likely be one of the most significant mechanism for corrosion in this system.
 - A small microchannel heat exchanger constructed by diffusion bonding needs to be tested under operational conditions with supercritical CO₂ and liquid sodium.
 - Most or all of the work can be performed at the existing facilities at Argonne National Laboratory.



Flowing Sodium Cooled by Air Flowing Over Test Section Causing Precipitation of Sodium Oxide on Wall

1,800 cubic feet per minute (cfm) air blower with variable frequency drive for controlling air velocity and chiller

Test section and heaters inside of stainless steel air duct half-wall

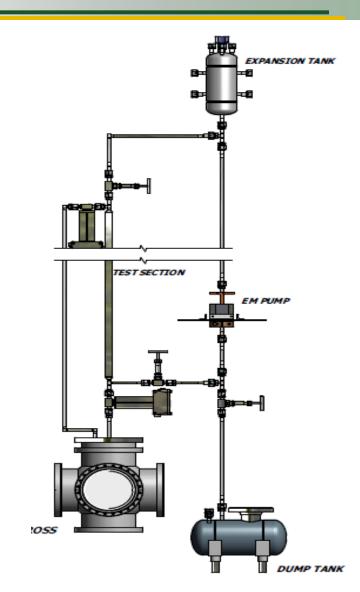






Small-Scale Sodium Drain and Fill Tests

- In case of sodium leak, intermediate sodium circuit normally drained of sodium to limit spillage and sodium fire
 - Seek drain time of about 15 minutes
 - Small sodium channels of compact heat exchangers must be demonstrated to drain efficiently
- Test section is contained on a tilting assembly such that the orientation can be varied from vertical to horizontal
- Test section drains into a six-way cross
- Test section drained under Argon
- Test section is instrumented Ultrasonic detection of time dependent draining film thickness to be investigated
- Various test sections with different channel geometries
- Sodium loop for wetting of stainless steel by sodium prior to tests





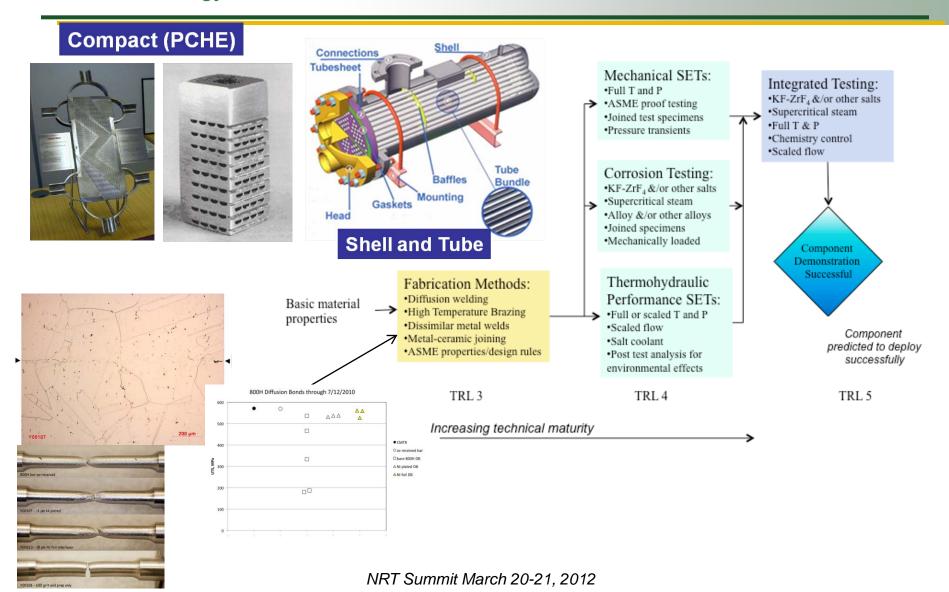
Fundamental Sodium-CO₂ Interaction Tests

- Small-scale sodium facility is being assembled to provide fundamental data on interactions between sodium and CO₂ released into sodium through stainless steel micro-leak configurations and self-plugging of stainless steel micro-leak configurations under realistic conditions of sodium-to-CO₂ heat exchanger failure
- Envisioned failure mode for compact diffusion-bonded heat exchangers involves formation of microcracks limiting flow of CO₂ into sodium with possibility of self-plugging of crack channels due to formation of solid reaction products





Technology Development

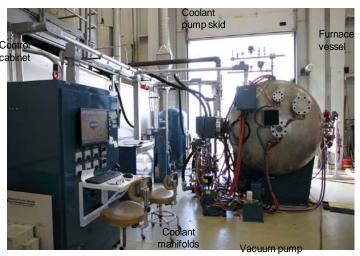




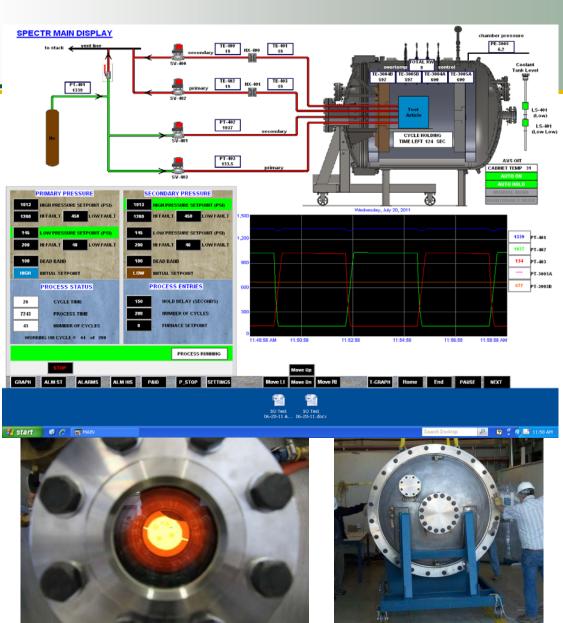
SPECTR:

Single effects testing of cyclic pressure transients at operating temperature

- •Demonstrates TRL 4 for SHX
- •Needed for ASME Section 3, HH qualification of diffusion welds
- •Potential savings of over \$250M



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Expected FY 2012 Accomplishments

- Install and commission the DOE-NE closed Brayton cycle TA at Sandia, Bldg 6630. Completing the 1st phase of the Sandia Nuclear Energy Systems Laboratory/Nuclear Technology User Facility/Brayton Systems Labs. (Low Pressure Closed Brayton Cycle, Supercritical Fluid Brayton Compressor Laboratory, and Split Flow-Fully Recuperated Supercritical CO2 Brayton Cycle). Release produced power to local grid.
- Adapt Brayton Laboratory to the customer cycle and generate results and report that justify continued funding for FY 13 from the industry customers.
- Begin In-depth Corrosion Studies and Domestic Compact Heat Exchanger Development
- IF DOE-EERE SunShot proposal is funded, perform initial sizing and configuration studies. Evaluate Sandia NTUF/Phase 2 as a 10 MWe TA site host. Power to be delivered to local grid
- Initiate EPRI power study
- Complete conceptual design of SEP and initiate Phase 2.



ANL Energy Conversion Technology Team

- Jim Sienicki
- Anton Moisseytsev
- Rick Vilim
- Yoichi Momozaki
- Dave Chojnowski
- Dae Cho
- Claude Reed
- Craig Gerardi
- Dennis Kilsdonk
- Mitch Farmer



INL Energy Conversion Technology Team

Molten Salt Reactor Heat Exchanger

- Michael G. McKellar
- **■** Piyush Sabharwall
- Denis Clark



Supercritical Carbon Dioxide Brayton Cycle Development at Sandia National Laboratories

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■ Sandia Brayton Cycle Team

ARC Team SEP Team

Jim Pasch – PI Bobby Middleton – PI

Tom Conboy – Lead TAC Engineer William Martin – Brayton Systems Engineer

Darryn Fleming-Lead Mechanical Engineer David Ames – Lead Systems Engineer

Robert Moore – Lead Chemical Engineer Julius Yellowhair – Solar Receiver Engineer

Robin Sharpe – Lead Technologist

Bob Fuller – BNI, PI

Industrial Development Team

SMR Team

?- PI

?- Lead TAC Engineer

? - Lead Mechanical Engineer

? – Lead Chemical Engineer

? – Lead Technologist

? - BNI, PI

Gary Rochau - Pl

Angie Dyke/Sarah Hannigan – Financial Analysis

Bianca Thayer – Licensing Executive

Brooke Marshall – Technology Transfer Executive

Laura Dalton - Non Disclosure Agreements

Lynette Rocheleau – Copyrights

Dan Jenkins - Patents



Commercialization Approach

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Secure Intellectual Property

- Export Control Determination
- US Competitiveness Determination
- Patents
- Patent Disclosures
- Copyrights

Announcement of Intent to Collaborate

- Federal Business Opportunities
- Non-Disclosure Agreements
- S-CO2 Symposium

Development of Collaboration Tools

- Cooperative Research and Development (Funds-In)
- Work For Others Agreements (Private Contracts)
- Joint Proposals (responding to Broad Area Announcements)

Establish Nuclear Technology User Facility

- Gain square footage for user defined experiments Leveraging legacy remediation
- Establish capabilities supporting experiments (S-CO2 loops, models, technical support)
- Financial Processes to support user defined experiments (Using solar test facility models)



Technology Development Efforts

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DOE-EERE Sunshot FOA proposal

- NREL, EPRI, and industry participants
- 10 MWe SCO2 Brayton technology NG Heated
- Concentrated solar power applications with dry cooling.
- Power Returned to local Grid
- DOE-NE Brayton cycle Test Assembly(TA) testing capabilities at Nuclear Technology User Facility(NTUF)
 - Reconfiguration of Sandia Brayton Loops
 - Likely established NTUF's first commercial customer
 - First test results required by October 1, 2012.
 - Specific objectives for near-, mid-, and long-term testing of the TA are being developed.
- Risks to the smooth and continued access to TA testing are being identified, and contingency plans developed to minimize down time.







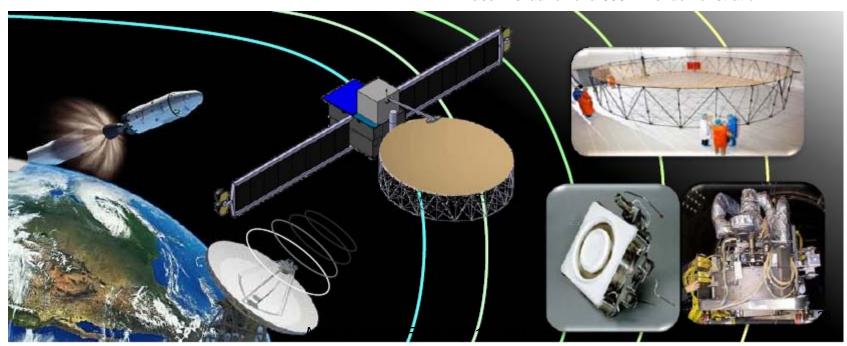
Technology Development Efforts (Continued)

- GE-Global funding project for development of a 10 MWe bottoming cycle for Gas Turbines
 - User facility application in initial phase
 - Configuration is DReSCO
- Collaborating with EPRI on mutually beneficial studies regarding the application of SCO2 closed Brayton power conversion concepts to traditional EPRI customers
 - Coal-fired (including current and future Ultrasupercritical Steam Plant designs)
 - Concentrated Solar Thermal
 - Geothermal
 - Nuclear
 - Topping and bottoming cycles.
- Collaboration with EPRI includes
 - Exhaustive literature search
 - Theoretical cycle performance modeling
 - Establishment of realistic performance specifications of the major cycle hardware components



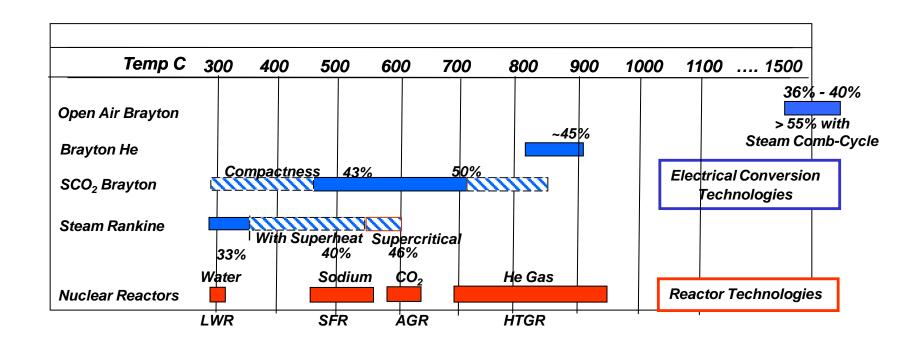
Technology Development Efforts (Continued)

- Cooperative Research and Development Agreement signed with Northrup Grumman-Aerospace
- Development of a Solar-Electric-Propulsion (SEP) for space tug applications to move satellites from low earth orbit to high earth orbit.
- Phase 1 is development of a conceptual design at TRL level 3
 - Low Pressure Brayton Loop is prototype (He-Xe)
 - Concentrated Solar heat exchanger is the critical component
 - 3 month time line
- Phase 2 is construction of prototype hardware for earth base demonstration to take technology to TRL level 7-8
 - 2 year time line
- Phase 3 is launch of a 150 KWe demonstration
- Phase 4 is launch of a 300 KWe demonstration





Power Conversion and Nuclear Reactor Outlet Temperature Ranges

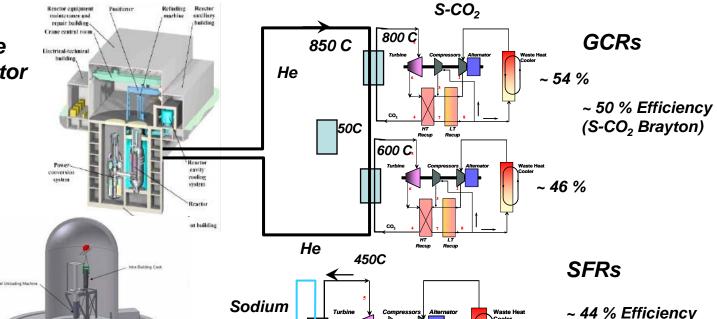


S-CO₂ Power Conversion Operating Temperatures Matches all Advanced Reactor Concepts LWR – compactness, condensing cycle appear promising



S-CO₂ Power Cycles for Reactors

NGNP High Temperature Gas Cooled Reactor 850-900 C

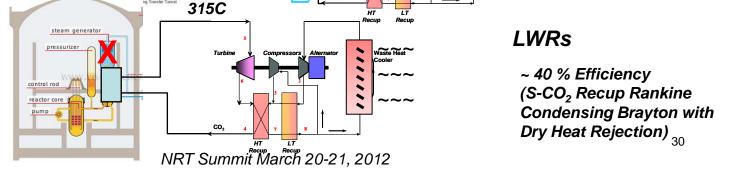


525C

Sodium Cooled Reactor 500-550 C

LWRs Pressurized Water Reactor 330 C

Potential SMR Applications



(S-CO₂ Brayton)